



Engine Fuel Production from Waste plastic Pyrolysis (WPO) and Performance Evaluation in a CI engine with Diesel Blend

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Abstract

Plastic waste disposal throughout the world is creating problems and degrading the environment. Today transportation and electric power generation in rural areas mostly depend on fossil fuels. Such extensive use of fossil fuel is resulting in depleting it at an alarming rate. Hence, it is required to produce an alternative fuel to keep them running as well as minimizing waste disposal. Waste plastic pyrolysis oil is identified one of such good alternative. In this study, waste transparent plastic, used for packaging, is used for the conversion of fuel through pyrolysis process. It was observed that yield of plastic oil was approximately 65-70 %. However, a liquid yield affects heating rates and heat loss patterns in the reactor system. This paper also presents the effect of waste plastic pyrolysis oil in a diesel engine at various compression ratios with different load and blending with pure diesel (pure diesel, 10%, 20%, 30%, 40%) at constant engine revolution. The performance characteristics include engine brake power, brake thermal efficiency, specific fuel consumption and exhaust emissions. Experimental investigation shows that Plastic oil can be used to save the 40% diesel without loss of power, and its trend do not differ with variation in compression ratio.

1. Introduction

Energy, environment and economy are one of the major contributors for developing the country. Fossil fuels are depleting day by day, which results in rise of petroleum products prices around the globe. This indicates requirement of an alternative cheaper fuel to fulfil the need of transportation, and electric power generation in the rural area. On the other hand, waste product generated with growth of population and its management plays essential role to maintain economic and healthy country. Among many types of Solid waste, plastic waste is a major problem as its non-biodegradable in nature. Plastic usage has become crucial part in today's world, because of their lightweight, durability, non-perishable nature, faster rate of production and flexibility in design and the demand of commodity [1,2]. In general, plastics are formed using petroleum products and consists of long hydrocarbon chains. These contain many additives such as colouring agents, anti-oxidants and stabilizers [3,4]. High-density polyethylene is a highly used plastic after poly vinyl chloride (PVC) and polypropylene (PP) [5]. Plastics are non-biodegradable polymers and remains more than 100 of years, adding significantly to the problem of waste management [6,7]. Moreover, the huge demand for plastic has created a large amount of plastic waste and its consequences are serious threat to the environment due to its disposal problems. The toxic substances released are causing a threat to vegetation, animal and human health and environment as a whole. In detail, burning of plastic wastes increase the risk of heart disease, aggravates respiratory ailments such as asthma and emphysema and cause rashes, nausea or headaches, and damages the nervous system [1]. According to a survey carried out in India, it found that annual consumption of plastic was nearly 8 million tonnes. Around 70% of this is recycled and remaining plastic waste is going as landfills [1,8]. Wastage of energy is the recent trend in the selection of alternate fuels [9,10]. Fuels and its

blend like alcohol, biodiesel, liquid fuels from plastics etc. are promising alternative fuels for the internal combustion engines [11]. As plastic is made of hydrocarbon, is cheap and easily available, and corresponding to tonnes of waste, leads us to consider it as an alternative fuel for engine. This could be an important tool to save the environment as well as stop plastic wastes accumulation. Considering this fact, many authors [11-13] had worked on oil extraction from plastics as an alternative source of fuels for the diesel engines. They proved that WPO fuel is capable to run both SI and CI mode of an engine. There are many methods to extract the waste plastic oil (WPO), among them pyrolysis process is the most common process to obtain the production of fuel. Author [14] produced WPO through waste plastic by initially crushing into small pellets, transferring to the reactor for thermal degradation wherein the absence of air it is heated to the range of 300–900 °C and plastic vapor forms, which being condensed and finally collected as WPO. Shafferina et al. [15] reviewed and suggested that the yield of WPO through pyrolysis process strongly depends upon types of plastic and selection of catalytic. Furthermore, the yield also depends on temperature and duration of reaction. Miandad et al. [16] revealed that as reaction time increases beyond 75 minutes, yield decreases and tar content increases, also proposed that the optimum conditions for maximum liquid oil yield of 81% achieved at 450 °C temperature and 75 min reaction time.

Beside this, investigation of the optimum performance, emission and fuel consumption aspect of an internal combustion engine using WPO has similar importance. Panda et al., [12] experimentally observed that engine gives better performance up to 30%, while it may operate with maximum up to 50% waste plastic oil blended to diesel. The study shows a stable performance with brake thermal efficiency similar to that of diesel and its value is higher up to 80% of load. Also, observed that throughout the experiment, emissions are considerably higher than that of the diesel baseline. Anupet et al. [17] concluded that petrol engine fuelled with waste plastic pyrolysis oil exhibits higher thermal efficiency up to 50% of the rated power for petrol engine. Viswanath et al. [8] performed experiment and revealed that the higher calorific value and more oxygen content of WPO significantly increases heat release rate than diesel, however possession of high viscosity with blends, leads to poor atomization, long ignition delay and combustion duration in compare to diesel at full load. In addition, Mani et al [6, 18] suggested that use of WPO, Ignition delay become longer by about 2.5° CA, NO_x is higher about 25%, CO 5% and Unburned hydrocarbon about 15%, and smoke reduced by about 40% to 50%. Ceyla et al. [19] also found the similar trend of emission. Injection timing for any CI engine plays major role for combustion and performance. Mani et al. [6] investigated that change from 23°bTDC to retarded injection timing of 14°bTDC lead to decrease oxides of nitrogen, carbon monoxide and unburned hydrocarbon. Viswanath et al. [20] experimentally investigated and found that brake thermal efficiency of blends are lower compared to diesel, but 25% blending shows similar performance to that of diesel.

There are many investigations have been done with respect to different proportion of blends with conventional diesel and types of engines. Compression ratio (CR) of an engine plays important role to enhance the efficiency and overall performance however, its performance investigation is inadequate. The effects of CR along with variation of load and blends on the combustion characteristics, emission, and specific fuel consumption not been investigated together adequately. Therefore, the purpose of this work is to obtain optimum performance of WPO blends with conventional diesel. Experimental investigation was conducted and the effect of engine performance parameters as brake thermal efficiency, brake power, specific fuel consumption, emissions using WPO and diesel of various blends like B10, B20, B30, B40 at different compression ratios and corresponding applied load were extensively studied.

2. Methodology

2.1 Fuel preparation by pyrolysis:

Waste plastic pyrolysis oil involves subjecting plastic to high temperature for the treatment of chemically decomposing of organic materials in absence of oxygen, otherwise it starts burning. During the process, initially plastic wastes have been cracked gently by adding catalyst, and the gases condensed in a series of condensers to give a low sulphur content distilled WPO. All this happens continuously to convert the waste plastics into fuel. The catalyst used in this system prevents formation of all the dioxins and Furans (Benzene ring). Figure 1 illustrates The laboratory scale pyrolysis setup consisted of a batch reactor sealed at one end and an outlet tube at the other end. An electric furnace used to provide heat to the reactor externally, and 20 gm of waste plastic sample was loaded in each pyrolysis reaction. The condensable liquid products (WPO) collected through the condenser and weighed. After pyrolysis, the solid residue left out inside the reactor and weighed. Reaction have been carried out at different temperatures ranging from 400–500°C. The property of collected WPO was measured as shown in table 1.

2.2 Experimental setup

The experimental setup is shown in fig.2. The experimental setup consists of single cylinder, four stroke, multi-fuel, research engine connected to eddy current type dynamometer for loading. The engine specification: bore and stroke are 87.7 mm and 110 mm respectively, displacement volume 661cc, opening and closing of intake valve at 45° b TDC and 35.5° a TDC respectively, exhaust valve opening and closing at 35.5° b BDC and 4.5° a TDC respectively, Fuel injection timing 23° b TDC at inlet manifold. The compression ratio can be varied without stopping the engine and without altering the combustion chamber geometry by specially designed tilting cylinder block arrangement.

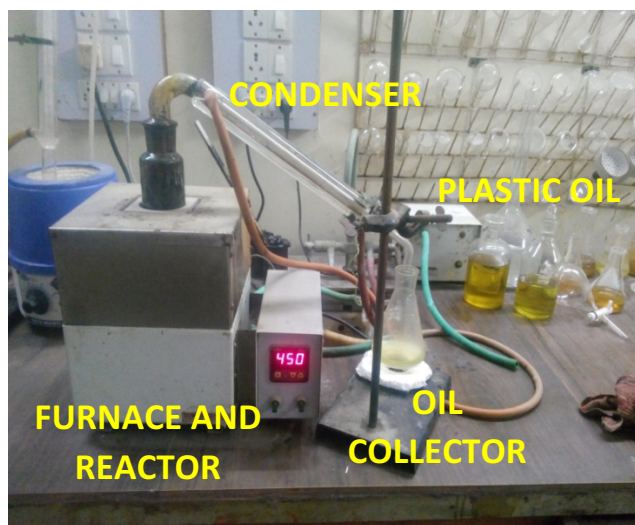


Fig. 1. Pyrolysis setup for WPO.

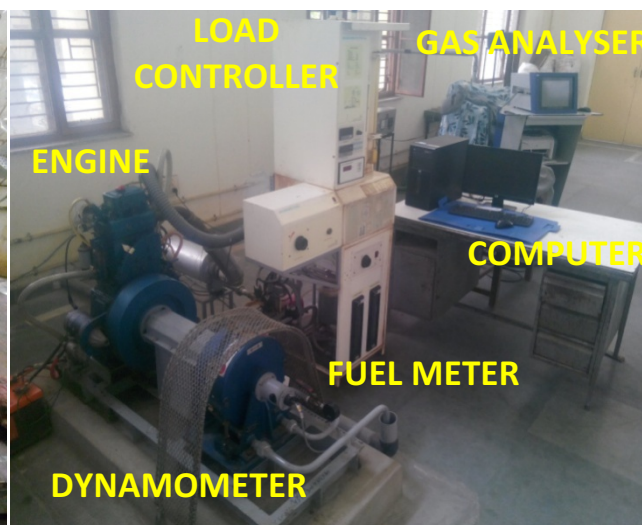


Fig. 2. Experimental set for engine performance.

Table 1: properties of waste plastic oil and diesel

Properties	Measuring Technique	B100(measured)	DIESEL(Pawar et al., 2013)
Density(kg/m ³)	Hydrometer cylinder	860	890
Calorific value (kJ/kg)	Bomb calorimeter	39500	42000
Flash point(°C)		36	>52
Fire point(°C)		41	>55

In Diesel mode fuel injection point and pressure can be manipulated for research tests. Air temp, coolant temp, Throttle position and trigger sensor are connected to Open ECU which control ignition coil, fuel injector, fuel pump and idle air. Set up is provided with necessary instruments for combustion pressure, Diesel line pressure and crank-angle measurements. These signals are interfaced with computer for pressure crank-angle diagrams. Instruments are provided to interface airflow, fuel flow, temperatures and load measurements. The setup has stand-alone panel box consisting of air box, two fuel tanks for duel fuel test, manometer, fuel measuring unit, transmitters for air and fuel flow measurements, process indicator and hardware interface. Rotameters are provided for cooling water and calorimeter water flow measurement. A battery, starter and battery charger is provided for engine electric start arrangement. The setup enables study of VCR engine performance for brake power, indicated power, frictional power, BMEP, IMEP, brake thermal efficiency, indicated thermal efficiency, Mechanical efficiency, volumetric efficiency, specific fuel consumption air fuel ratio, A/F ratio, heat balance and combustion analysis. Lab view based Engine Performance Analysis software package Enginesoft provided for on-line engine performance evaluation. All the experiments with different fuel ratios conducted for a constant engine speed of 1500 rpm and with varying CR and load on engine. Water flow through engine adjusted to 230 LPH and 90 LPH through calorimeter. Load varied from 0.0 kg to 12 kg corresponding to zero load to full load. All the performance and emission characteristics were determined by averaging 10 consecutive cycles. For exhaust gas, AVL DiTEST CDS 440 gas analyzer was used. The details of measuring equipment used and its accuracy level are listed in table-2.

3. Results and Discussions

3.1 Brake Power

Figures 1.1, 1.2, 1.3 and 1.4 show the variation of brake power with respect load applied. It indicates that the Brake power increases with increase in load, which is due to increase in amount of fuel to maintain the constant RPM corresponding to load increase. These figures conclude that blending of waste plastic oil

(WPO) with pure diesel are very close trend with pure diesel corresponding to variation of load. Figures also indicate that plastic oil is safer to save the 40% diesel without loss of power, and its trend do not differ with variation in compression ratio.

Table 2. List of measuring equipment used.

Instrument	Measurement	Measurement Technique	Range	Accuracy
Tachometer	Engine speed	Magnetic Pick-up	1200-1500rpm	± 5rpm
Thermometer	Temperatures	K-Type Thermocouple	0-1200°C	± 2°C
Eddy current type Dynamometer	Load	Strain gauge type	0-50kg	± 0.1kg
Pressure Transducer	Pressure	Piezo sensor	0-5000psi	± 2psi
AVL DiTEST CDS 440 gas analyzer	Nitrogen oxides	Electrochemical sensor	0-5000ppm vol.	± 5 ppm vol.
	Carbon monoxide	NDIR	0-15% vol.	< 15.0 % vol.: ± 0,02 % vol.
	Carbon dioxide	NDIR	0-20% vol.	< 16.0 % vol.: ± 0, 3 % vol. ≥ 16.0 % vol.: ± 5 % o.M.

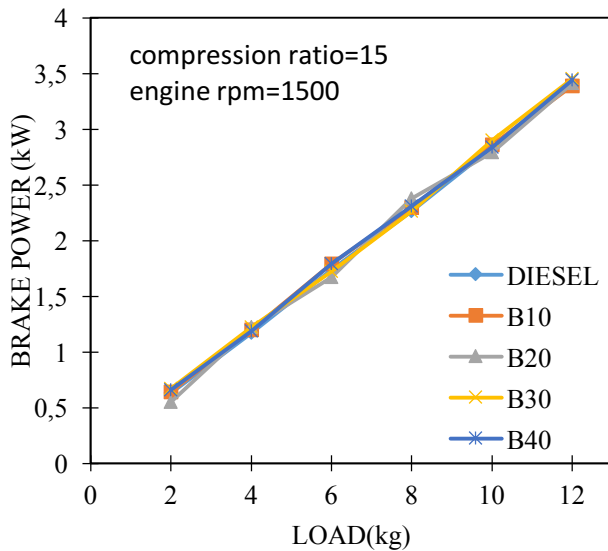


Figure1.1 Variation of brake power with load applied and blends

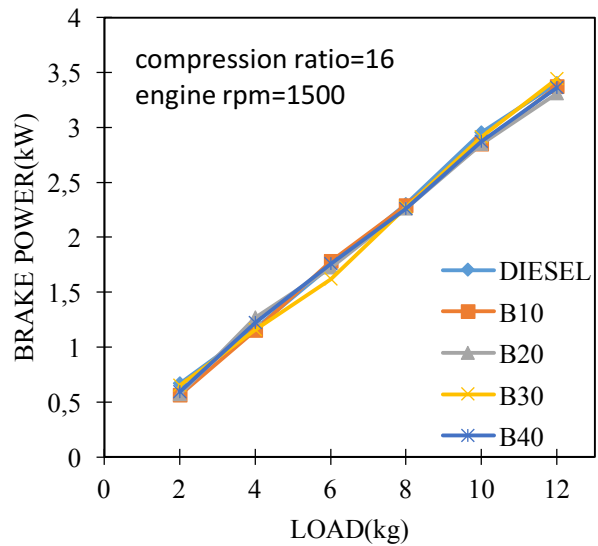


Figure1.2 Variation of brake power with load applied and blends

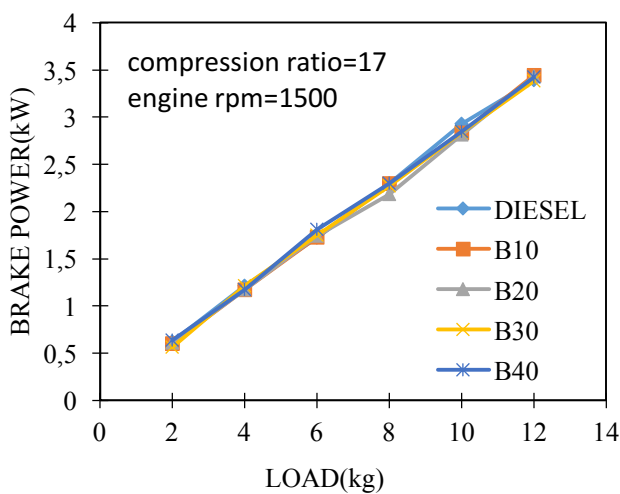


Figure1.3 Variation of brake power with load applied and blends

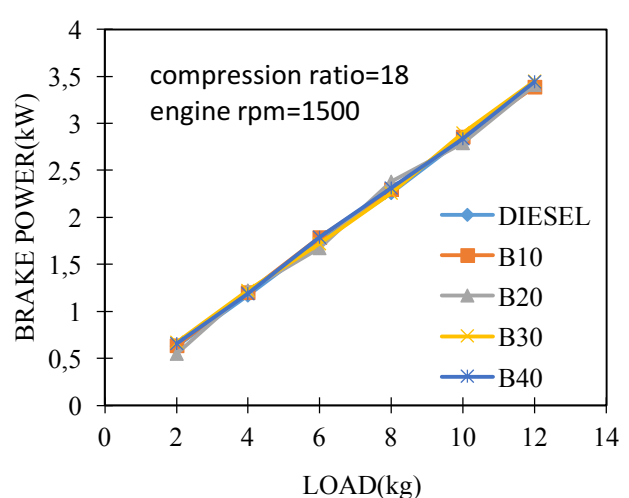


Figure1.4 Variation of brake power with load applied and blends

3.2 Brake thermal efficiency

Brake thermal efficiency (BTE) signifies how efficiently engine is capable to convert fuel into mechanical energy. Figures 2.1, 2.2, 2.3 and 2.4 illustrate the graph between the brake thermal efficiency and load applied from no load to full load corresponding to 0.0 to 12.00kg. It shows that the variation of brake thermal efficiency with compression ratio of 15, 16, 17 and 18. The brake thermal efficiency tends to be the same at lower load for all blends to the compression ratio of 15, 16 and 17, however, it varies for compression ratio 18. Brake thermal efficiency (BTE) increases with respect to increase in load, compression ratio, blending ratio up to 40%, and for all blend. However, the gap of BTE of diesel and blended fuels are deferent. Figure 2.1 shows maximum BTE at full load for diesel and B40 are 33.54% and 38.18% respectively at CR 15. Figure 2.2 shows that at maximum load BTE for diesel and B40 are 33.2% and 37.76% correspondingly at CR 16. at maximum load, BTE for diesel and B40 are 33.15% and 38.47% respectively at CR17. Figure 2.4 shows that at maximum load BTE for diesel and B40 are 33.33% and 38.7% at CR 18. This may be due to possession of higher calorific value of WPO and its blends with diesel then pure diesel (Panda et al.2016).

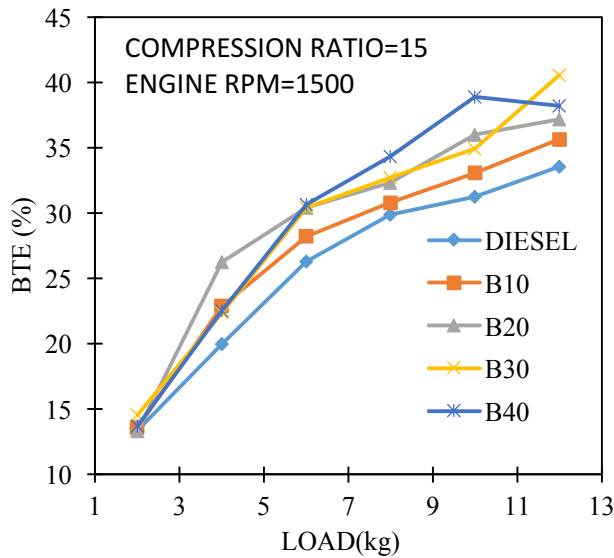


Figure 2.1 Variation of brake thermal efficiency with Load and blends

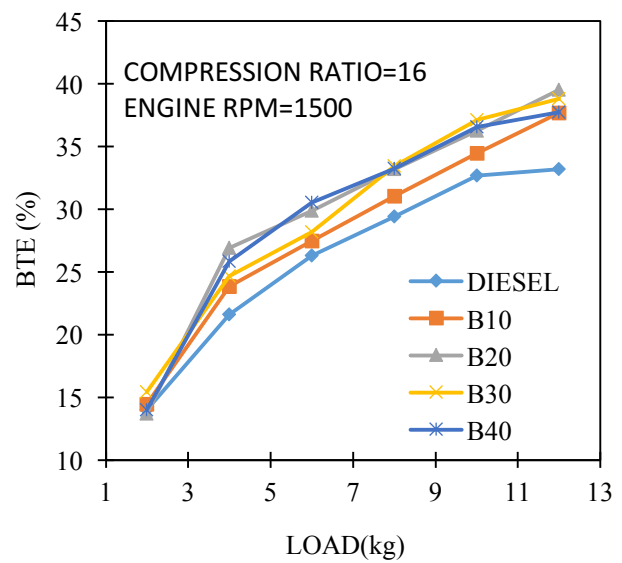


Figure 2.2 Variation of brake thermal efficiency with Load and blends

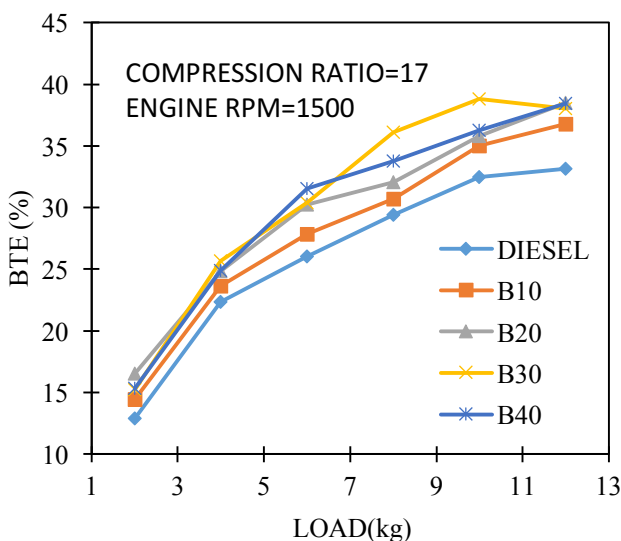


Figure 2.3: Variation of brake thermal efficiency with Load and blends

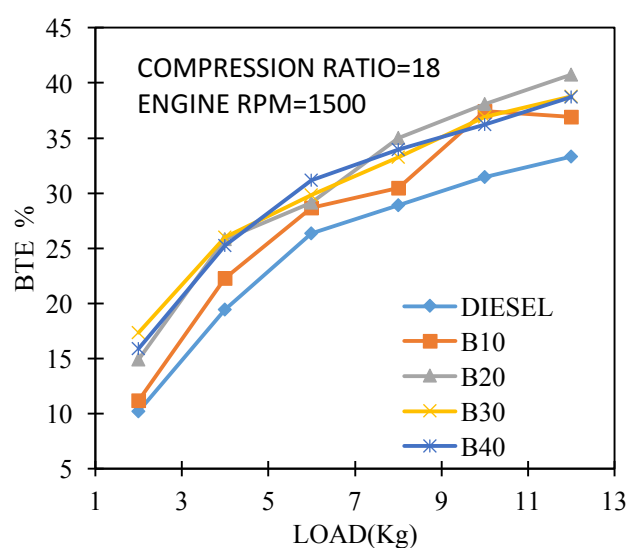


Figure 2.4: Variation of brake thermal efficiency with Load and blends

3.3 Specific fuel consumption

Figures 3.1, 3.2, 3.3 and 3.4 represents about the variation of brake specific fuel consumption (BSFC) with respect to different load applied in kg up to full load equivalent to no load - full load, and compression ratio of 15, 16, 17 and 18. These graph prove that as the load increses, BSFC decreases continously for all blends

and to all compression ratio. This is because, when the load increases temperature inside the cylinder increases, reduces delay period, total combustion timing increases and result proper combustion of fuel. It can also be noticed that trend of falling BSFC corresponding to load applied is almost same for pure diesel and B40 blend, however it differs for lesser ratio of blend and lower load. The variation in BSFC at maximum load for diesel and B40 is 0.26 ± 0.04 kg/kWh. Moreover, compression ratio 17 and 18 provide lesser BSFC of B40 blend at low load in comparison to CR 15 and 16. These trends of BSFC is all because of possessing high calorific value of WPO and better combustion toward higher compression ratio.

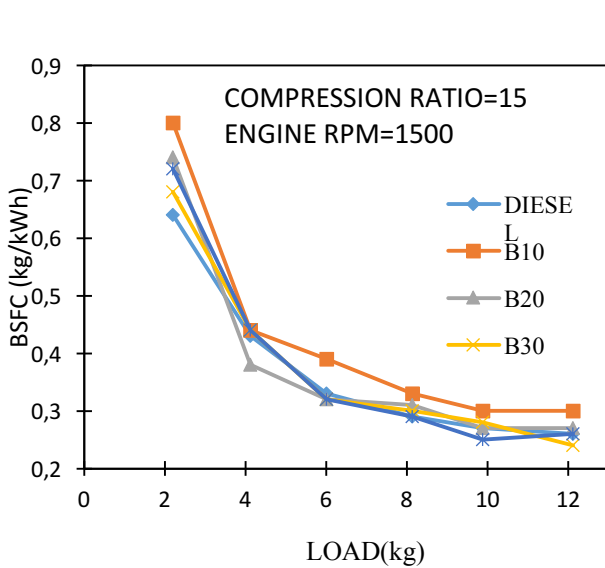


Figure 3.1: Variation of BSFC with Load and Blends

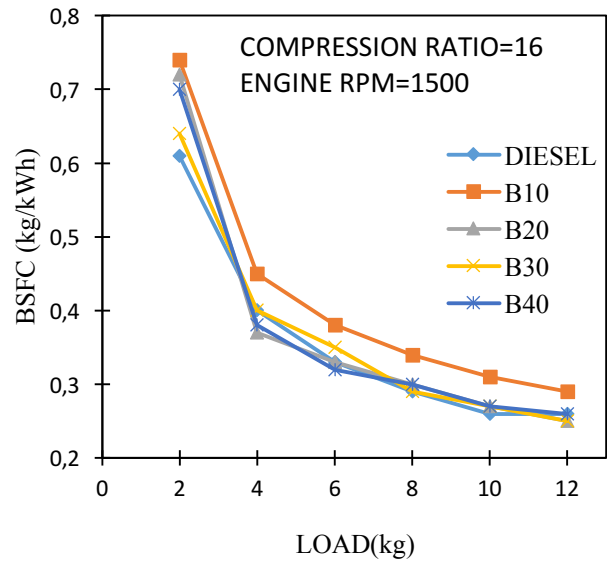


Figure 3.2: Variation of BSFC with Load and Blends

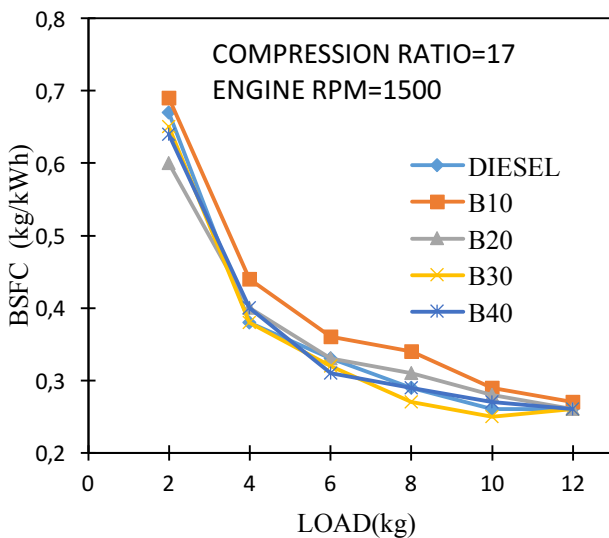


Figure 3.3: Variation of BSFC with Load and Blends

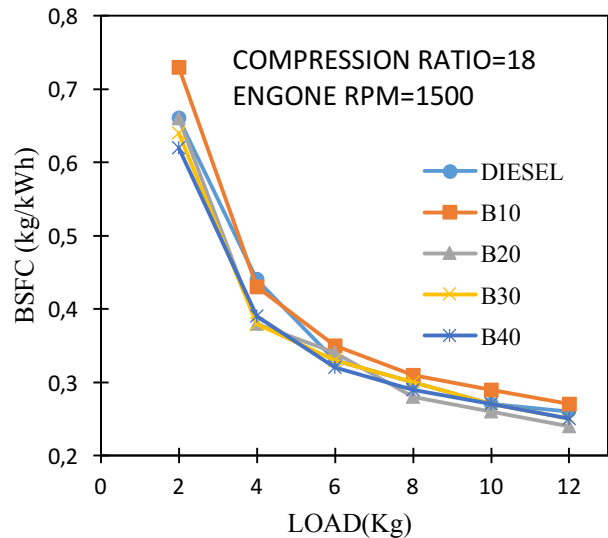


Figure 3.4: Variation of BSFC with Load and Blends

3.4 CO emissions

A toxic gas Carbon monoxide (CO) emitted from the engine, measured at tail pipe corresponding to variation of load, and at compression ratio of 15, 16, 17 and 18 are shown in the figures 4.1, 4.2, 4.3 and 4.4 respectively. The CO produced during the combustion due to lack of oxygen, poor air entertainment, mixture preparation and incomplete combustion (Heywood, J.B., 1984). It observed that Carbon monoxide (CO) decreases with increase in load, blend ratio up to 40% of WPO, and compression ratio. CO emissions decreases continuously for all blends, and the value of emission in volume percentage for B40 and pure diesel at maximum load are 0.04 and 0.03, 0.03 and 0.02, 0.02 and 0.02, 0.03 and 0.01 corresponding to CR 15, 16, 17, and 18 respectively. The reason behind decreased CO emission may be due to increase in combustion efficiency and better mixing. It can be noticed that the decreased in the value of CO emission with increase in load, blending ratio, and compression ratio fall are in the range of 0.13 to 0.01 volume percentage.

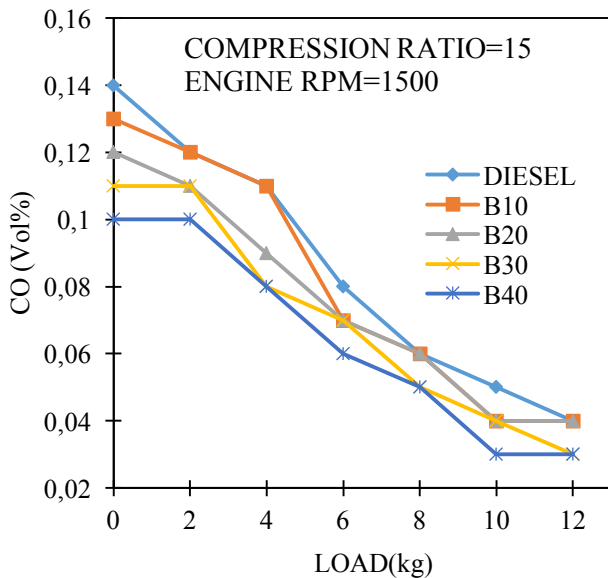


Figure 4.1: Variation of CO with Load applied and Blends

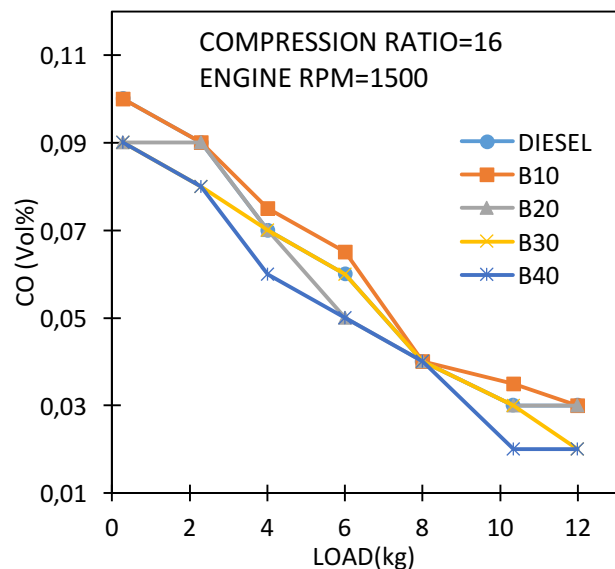


Figure 4.2: Variation of CO with Load applied and Blends

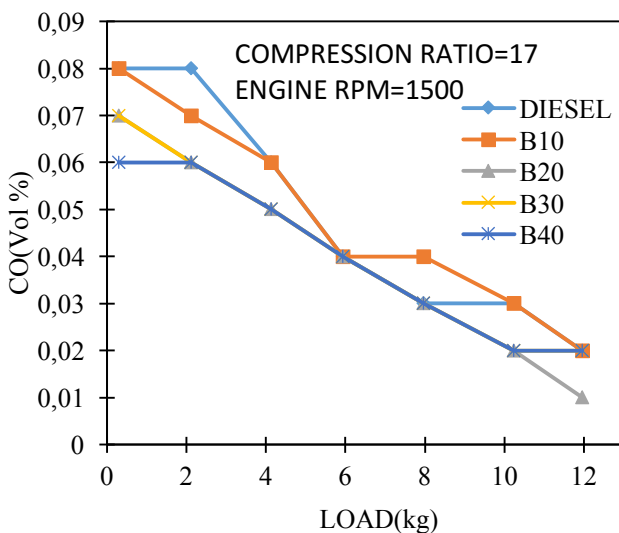


Figure 4.3: Variation of CO with Load applied and Blends

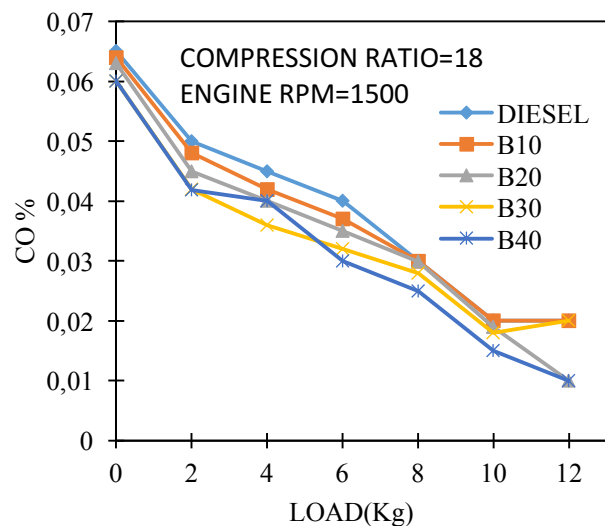


Figure 4.4: Variation of CO with Load applied and Blends

3.5 NO_x emissions

NO_x emission at the exhaust tail of an engine have been measured in parts per million (ppm) for different blends of WPO with pure diesel and with the variation of compression ratio (CR) from 15-18 are plotted as function of load in figures 5.1, 5.2, 5.3 and 5.4. The reason of NO_x formation is mainly due to availability of oxygen, reaction time and higher temperature during combustion. Figures depict that NO_x emission increases upto 10 kg (80% load) and decreases thereafter for the compression ratio 15 and 16, however, increasing trend of NO_x is continue for CR 17 and 18 throughout the load range. It can be observed that NO_x emission of B40 is very closed to pure diesel at lower load up to the 50% and higher for further increased load for all CR. Increasing of NO_x with load and blends increment might be due to higher heat released and higher combustion temperature. Moreover, could be due to longer ignition delay owing to the presence of long chain carbon compounds in WPO (Panda et al., 2016). Figure show that at maximum load NO_x emission for diesel and B40 is 316ppm and 282ppm respectively for CR 15, 321ppm and 294ppm for CR 16, 382ppm and 305ppm for CR 17 and 472ppm and 468ppm for CR 18. Which indicates NO_x emission is proportional to the CR increase, along with load and all blends.

3.6 CO₂ emissions

Increasing tendency of CO₂ emission corresponds to the complete combustion, however CO emission shows incomplete combustion. CO₂ emission decreases corresponding to increasing thermal efficiency. CO₂ exhaust

emission measured at exhaust tail at different blends (B10,B20,B30,B40) and compression ratio (15,16,17 and 18) with respect to load applied are shown in figures 6.1, 6.2, 6.3 and 6.4.

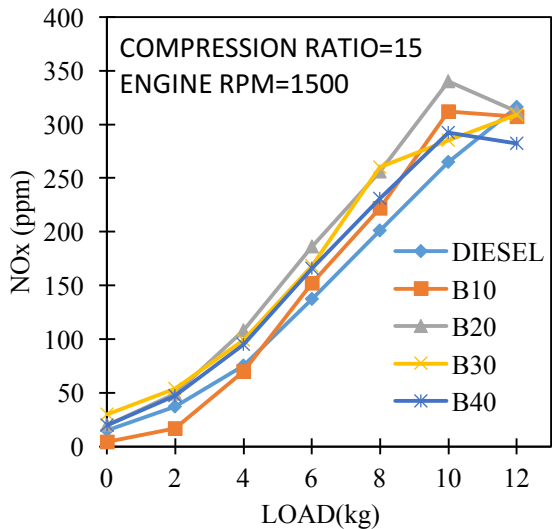


Figure5.1: Variation of NOx with Load and Blends

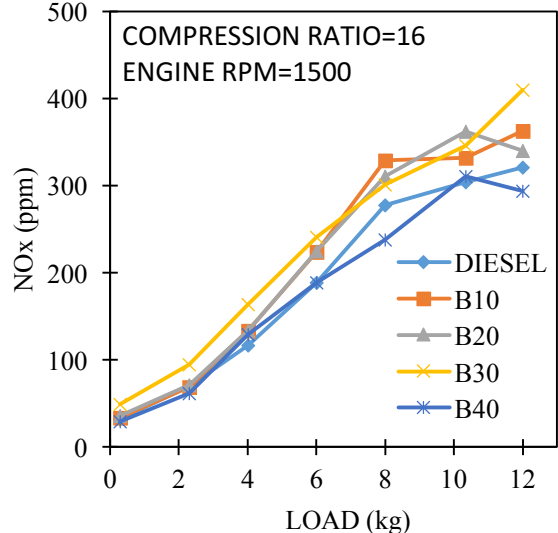


Figure5.2: Variation of NOx with Load and Blends

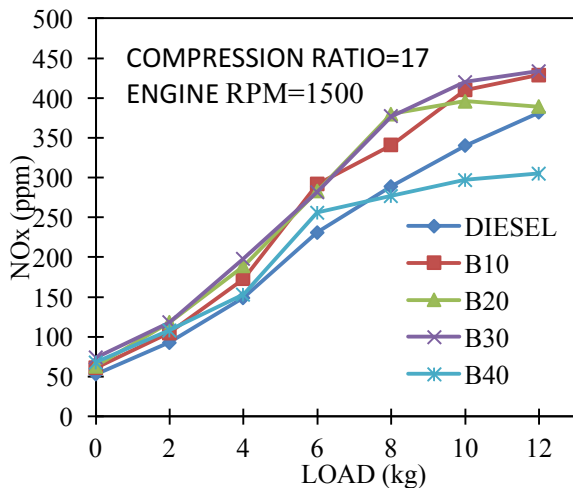


Figure5.3: Variation of NOx with Load and Blends

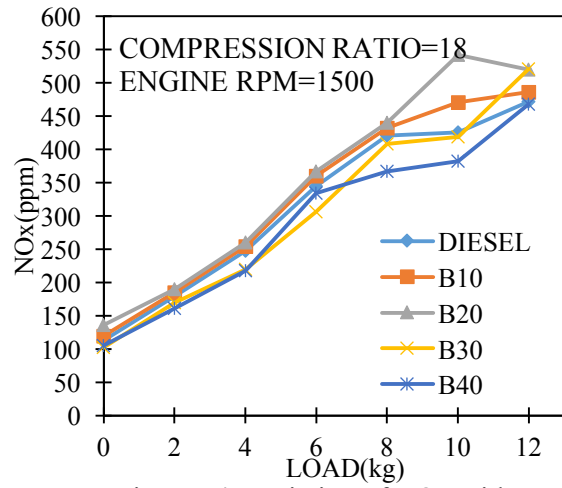


Figure5.4: Variation of NOx with Load and Blends

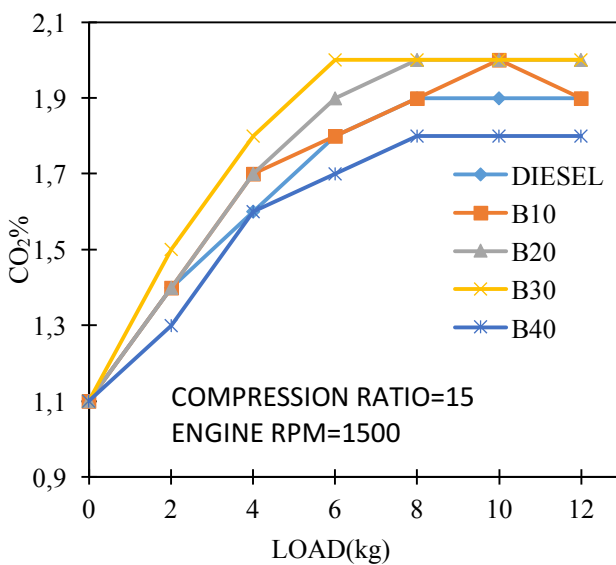


Figure 6.1: Variation of CO₂ with Load and Blends

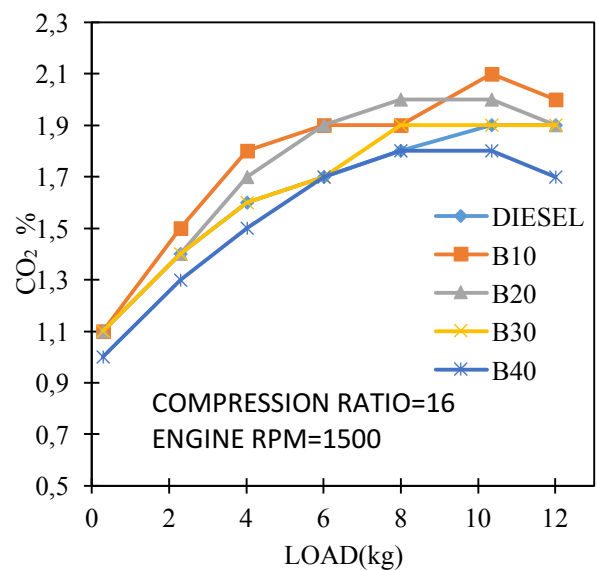


Figure 6.2: variation of CO₂ with Load and Blends

Figures illustrate that CO₂ emission of B40 is lower for all compression ratios, when compared with diesel. CO₂ emissions increase with respect to load for all blends, and at maximum load, emission for diesel and B40 is almost same as 1.9% and 1.8% respectively at CR 15, 1.9% and 1.7% respectively at CR 16, 2.1% and 2.1% respectively at CR 18. The average emission of CO₂ increases sharply up to the 60% to 70% (8-10 kg) of load and further slows down. This indicates that after 60% load engine gives better performance, although CO₂ emission is high.

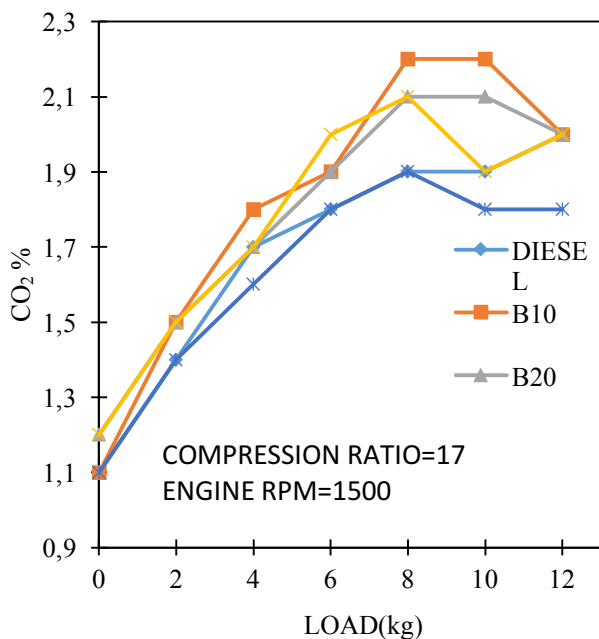


Figure 6.3: Variation of CO₂ with Load and Blends

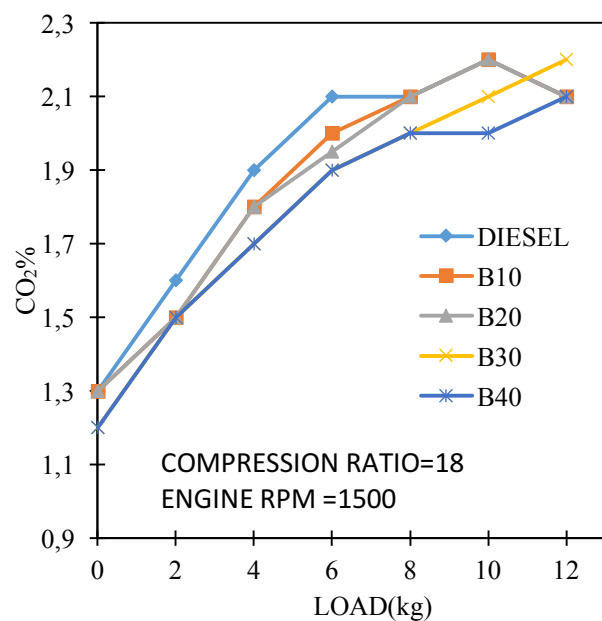


Figure 6.4: Variation of CO₂ with Load and Blends

4. Conclusion

An intensive experimental study was conducted on a single cylinder 4-stroke diesel engine to appraise the effects of performance and exhaust emission operating with WPO and its blends with diesel. The following conclusions are drawn from the experimental study

1. The use of Waste Plastic Oil blended fuel in a diesel engine causes improvement in engine performance and exhaust emissions. Plastic oil is save to use till 40% blended with diesel without loss of power, and its trend do not differ with variation in compression ratio.
2. Waste Plastic oil addition results in the increase of Brake Thermal Efficiency (BTE) and decrease in the specific fuel consumption. BTE for diesel and B40 are 33.33% and 38.7% at CR 18 at maximum load. The BSFC reduces with increase in CR. The variation in BSFC observed at maximum load for diesel and B40 is 0.26 ± 0.04 kg/kWh at CR 18.
3. Waste plastic oil addition results in significant reduction in exhaust emissions. Carbon monoxide (CO) decreases with increase in load, increase in blend ratio up to 40% of WPO and increase in compression ratio. NO_x emission of B40 is very closed to pure diesel at lower load up to the 50% and higher for further increased load for all CR. CO₂ emission of B40 is lower for all compression ratios, when compared with diesel. CO₂ emissions increase with respect to load for all blends, and at maximum load emission for diesel and B40 are almost same.

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