



## Bis thiourea phthalato Cobalt (II) complex: synthesis and studying as corrosion inhibitors for carbon steel alloy(C1010) in 0.1M HCl

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### Abstract

In this study of bis thiourea phthalato cobalt (II) complex (PTUCo) was synthesized and characterized by CHNS, FTIR, UV-Visible, Mass, TG and XRD techniques. The complex was evaluated as corrosion inhibitor for carbon steel alloy (C1010) against corrosive medium of 0.1M hydrochloric acid at 25°C and showed the efficiency 95.63% at concentration of 5 ppm. The effect of temperature on the inhibition behavior was studied at 35, 45 and 55 °C and the inhibitor reveals reducing in its efficiency as temperature raised, kinetic parameters like  $E_a$ ,  $\Delta H^*$  and  $\Delta S^*$  were calculated and depicted that increasing the activation of energy in presence of the inhibitor compared with the absence of the inhibitor. The inhibitor behaves as mixed inhibitor. The adsorption study insist that the inhibitor obey to Langmuir adsorption isotherm.

### 1. Introduction

Metals in general are widely used in industry, especially carbon steel which is considered as a material of choice, in addition it is often used as a construction material for chemical reactors, heat exchange systems and boiler, storage tanks, oil and gas transportation pipelines [1, 2] Metals require a pretreatment most of the time based on acidic solutions such as hydrochloric acid solution which is widely used in the industry: cleaning, stripping, acidification of oil, descaling and petrochemical processes. In the oil industry, 15% HCl is used for the acidification treatment, to solubilize the manipulations [3-5]. Metal's corrosion is an unavoidable difficulty for industries. In fact, corrosion occurs either by the two different metals or alloys, and also if that metal or alloy is present in corrosive environments, such as saline, basic or acidic media. [6,7]. Mild steel is the most extensively employed metal in industrial applications because of its excellent mechanical characteristics and inexpensiveness [8]. To treat the corrosion problems, there are several ways, one of them is used the corrosion inhibitors, For this, the using of inhibitor is one of the most trustworthy and economical method, that are chemicals when added in a suitable concentration are able to reduce the corrosion rate when present in the corrosion system without significantly changing the concentration of any other corrosive agent. The use of inhibitors during acid pickling procedure is one of the most practical methods for protection against corrosion in acidic media as well. Organic compounds containing hetero-atoms like N, O, S and P are famous compounds that

used as corrosion inhibitors for iron and its alloys especially for carbon steel alloy as for reduction of acid consumption occurring during the course of corrosion [9, 10]. Although, a great number of studies devoted to the subject of corrosion inhibitors, the development of corrosion inhibitors has always determined by their effectiveness, the complexes are tried to use as corrosion inhibitors for carbon steel alloy from many researchers [11-27]. thiourea, its derivatives and its complexes were used as corrosion inhibitors in industrial operations [28, 29]. In the present work, a novel complex bis thiourea phthalato cobalt(II) complex was synthesized to estimate as corrosion inhibitor against corrosive environment of 0.1M HCl on the carbon steel alloy C1010 surface.

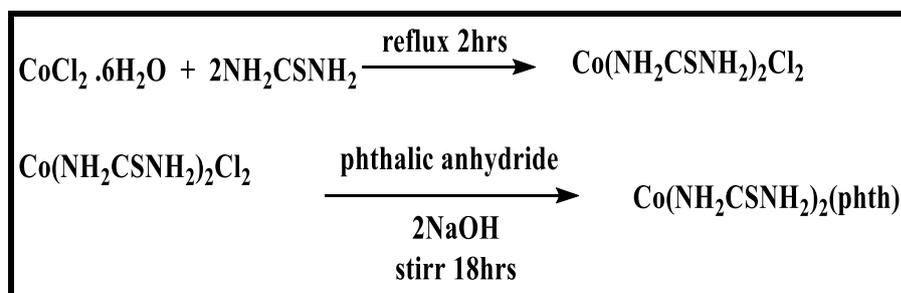
## 2. Material and Methods

### 2.1. Chemicals

The chemicals that used in this study were purchased from different companies, including: Ethanol(99.99 Scharlau), Hydrochloric acid(37Aldrich), Dimethyl sulfoxide (DMSO 99 Alpha), Dichloride methane(DCM 99 Fluka), Di ethyl ether (99.5 SCH), thiourea (99.99 Aldrich), Cobalt chloride( $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$  99.5GPR), Phthalic anhydride(99.5 GPR) .

### 2.2 Synthesis of bis thiourea phthalato cobalt (II) complex (PTUCo).

To a solution of  $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$  (10 g, 0.042 mol) in 100 mL of ethanol was added thiourea (6.384 g, 0.084 mol) dropwise. After the solution was reflux for 2h, a solution of phthalic anhydride (6.216 g, 0.042 mol) and sodium hydroxide (3.36 g, 0.084 mol) in 40 mL of water was added. The mixture was stirred for 18h and after cooling the violet precipitate filtered and washed by distilled water, absolute ethanol and diethyl ether. Washing of the complex was achieved by dissolving the solid with a minimum amount of dichloromethane and then adding a large excess of ethanol [30]. Leaving the solution undisturbed at room temperature for 24 h produced brown precipitate which were dried in vacuum. The melting point of the product is (<300°C decoms) violet color, Mwt ( $374.633\text{g}\cdot\text{mol}^{-1}$ ), Yield:4.1637g (26%). [31, 32]. Scheme (1) show the synthesis of the complex.



Scheme (1): Shows the Synthesis of PTUCo complex.

## 3. Characterization of the bis thiourea phthalato cobalt (II) complex (PTUCo):

**3.1. CHNS Element analysis:** The complex PTUCo was characterized by CHNS technique and the data shows matching between theoretical calculation and experimental, Table 2 show CHNS of complex.

Table 1 . CHN Element analysis of PTUCo

Co C <sub>10</sub> H <sub>12</sub> O <sub>4</sub> S <sub>2</sub> N <sub>4</sub>	C%	H%	N%	S%
Calculated	32.03	3.20	14.94	17.08
Found	32.01	3.21	14.88	17.05

### 3.2. FTIR spectroscopy:

the complex PTUCo was characterized by FTIR technique (KBr pellet,  $\text{cm}^{-1}$ ) in the region ( $400\text{--}4000\text{ cm}^{-1}$ ), the complex was given the following packages  $\nu_{\text{NH}}$ (3502)(assym), 3417 (symm),  $\nu_{\text{C=O}}$  (1688),  $\nu_{\text{NH}}$  (1566) (bending)),(1612)  $\nu_{\text{C=C( aromatic)}}$ ,  $\nu_{\text{COO}}$ (2200),  $\nu_{\text{C=S}}$ (1411),  $\nu_{\text{C-O}}$ (1153), and  $\nu_{\text{CN}}$  (1489),  $\nu_{\text{C-S}}$ (756) and out of plane bending  $\nu_{\text{N-H}}$ (702),  $\nu_{\text{Co-S}}$ (493),  $\nu_{\text{Co-O}}$ (705) [33-38]. Figure 1 show FTIR spectrum for PTUCo

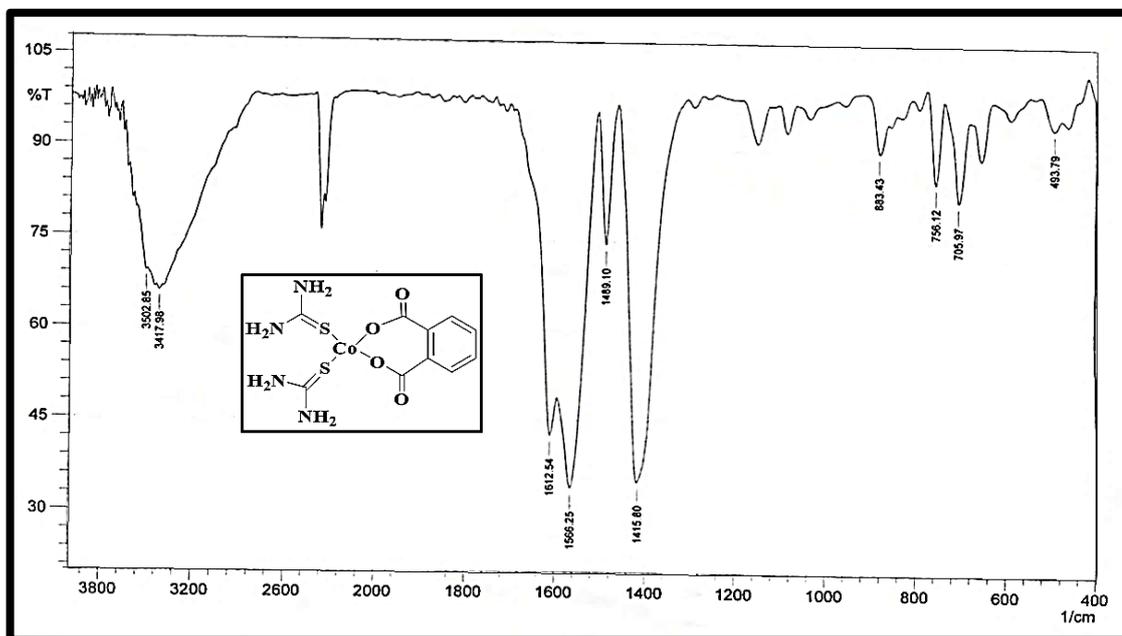


Figure (1): FTIR spectrum for PTUCo complex.

### 3.3. UV-Visible PTUCo complex:

The complex PTUCo was characterized by UV-Visible as shown in Figure 2 below where, Figure 2 revealed four transitions, 290 nm can be assigned to  $\pi \rightarrow \pi^*$  and  $n \rightarrow \pi^*$  in benzene ring and the two carboxylic groups that they ortho position one to another respectively. While the transition 335 nm is assigned to  $n \rightarrow \pi^*$  for C=S group and 405,435,580nm is assigned to d-d transitions [33, 39-41].

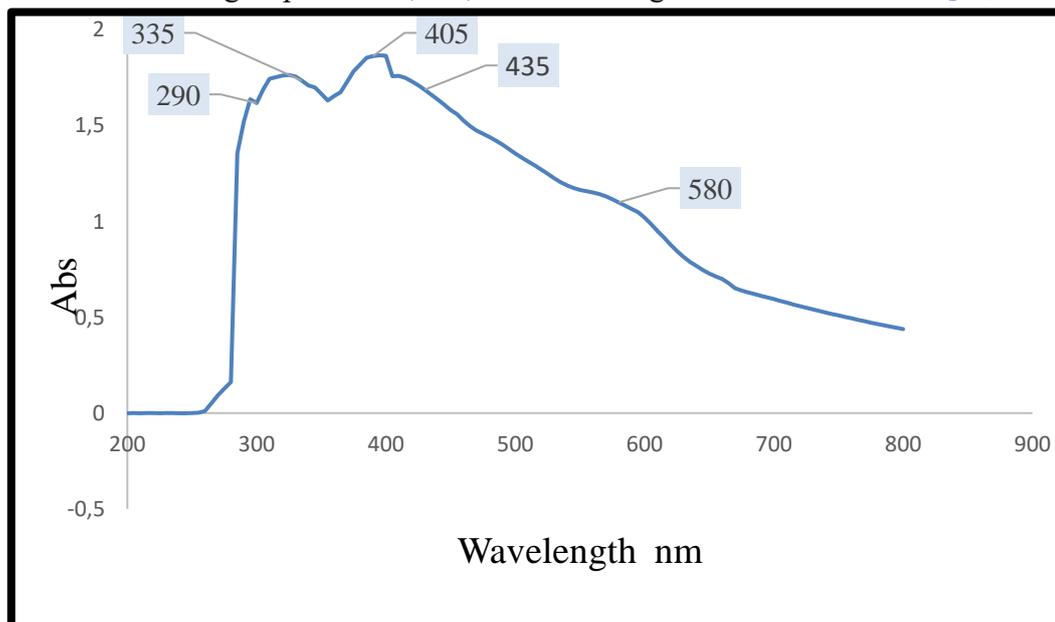


Figure 2: UV-Visible spectrum PTUCo complex.

### 3.4. Magnetic Susceptibility:

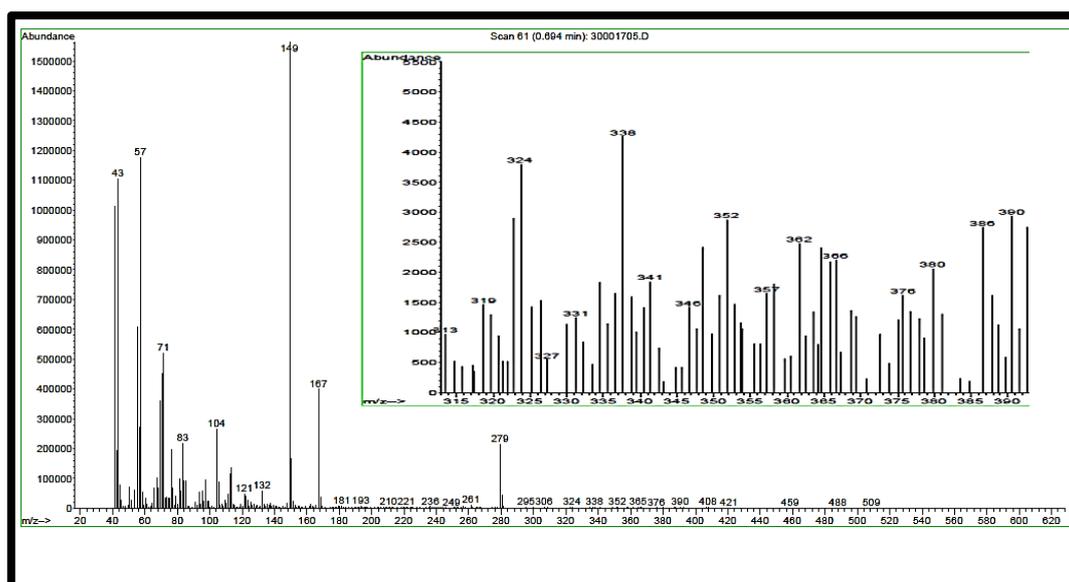
The magnetic moment of a complex was calculated and found to be equal  $\mu_{\text{eff}}$  3.9, where magnetic sensitivity calculations proved that the tetrahedral and cobalt oxidation state (2+)  $\text{Co}^{2+}$ . Table 2 that shows the molecular weight, magnetic moment coefficient, oxidation state and the geometry of the complex.

**Table 2. Magnetic Susceptibility of PTUCo complex**

Complex	Mwt	$\mu_{\text{eff}}$	Shape	Oxidation state
PTUCo	273.623	3.9	tetrahedral	+2

### 3.5. Mass spectra:

The complex (PTUCo) characterization by mass spectrum technique. Figure 3 Show the molecular ion peak at  $[\text{CoC}_{10}\text{H}_{12}\text{O}_4\text{S}_2\text{N}_4]^+$  which makes the structural formula and molecular weight of the complex and another important peak at 338 m/z can be assigned to the molecular ion  $[\text{CoC}_{10}\text{H}_5\text{O}_4\text{S}_2\text{N}_2]^+$  for the loss of two  $\text{NH}_3$  and hydrogen atoms H. and a peak at 324 m/z for the molecular ion  $[\text{CoC}_{10}\text{H}_5\text{O}_4\text{S}_2\text{N}]^+$  is attributed to the loss of the N nitrogen atom from the benzene ring and the beam bundle for the molecular ion  $[\text{H}_4\text{CoC}_2\text{O}_4]^+$  at 149 m/z due to the loss of the SCN thiocyanate root. The remainder of the benzene ring, as well as a peak at 104 m/z of the molecular ion  $[\text{HCoCO}_2]^+$  due to the loss of the  $\text{CO}_2$  molecule and two hydrogen atoms, in addition to the emergence of a peak at 57 m/z due to the  $\text{Co}^{2+}$  cobalt ion. [38].



**Figure 3:** Mass spectrum for PTUCo complex.

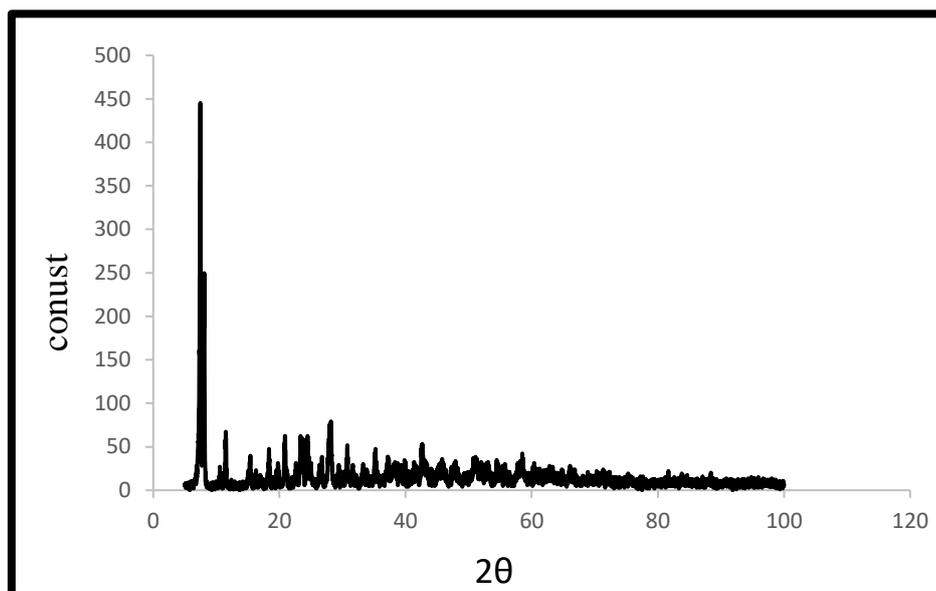
### 3.6. X-ray Diffraction (XRD):

The complex PTUCo characterized by XRD diffraction as in Figure 4 below where, it was used in the diagnosis of a complex (PTUCo) and the crystal size of the crystallization of the complex was calculated using the (Debye-Scherer) equation[33, 38, 42].

$$D = \frac{K\lambda}{\beta \cos \theta} \dots \dots \dots 1$$

where  $D$  is the crystallite size (nm),  $\lambda$  is the x-ray wavelength (0.15406 nm for  $\text{Cu K}\alpha$ ),  $K$  is the Scherer constant (0.9) that depends on the shape of a crystal,  $\beta$  is the full width at half maximum of intensity, and  $\theta$  is the Bragg angle, Figure 4 show XRD spectrum for PTUCo with a sharp peak at ( $2\theta=11.8144^\circ$ ),

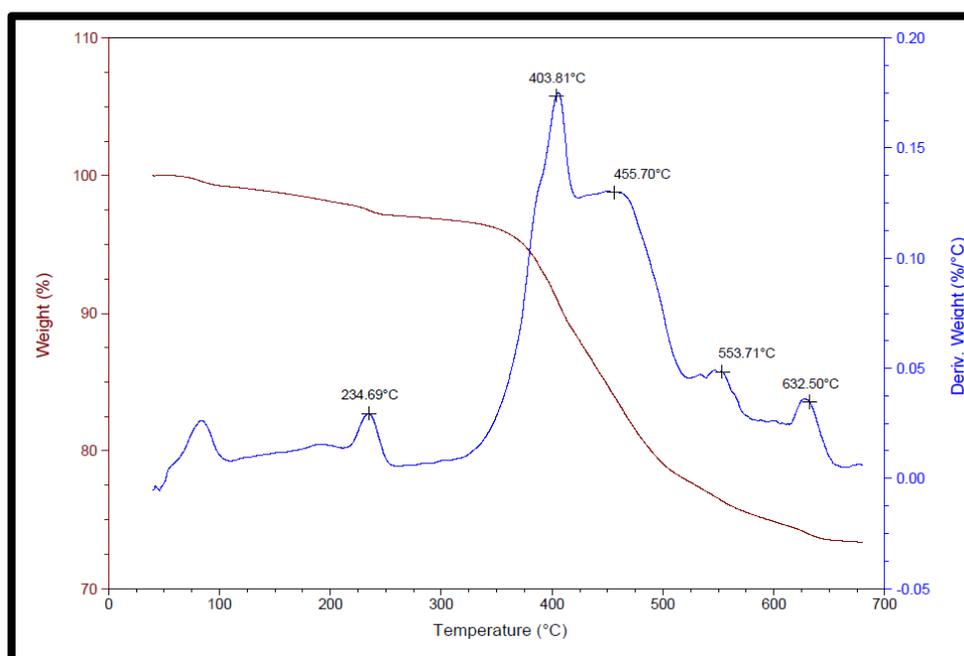
$\beta = 0.00314$  radian,  $D = 44.2374$  nm. It was observed from the crystal size calculation; the complex has a nano structure.



**Figure 4:** Shows XRD spectrum for PTUCo complex.

### 3. 7. Thermogravimetric Analysis:

In this study, Thermogravimetric analysis (TGA-DTG) technique was used to study the stability for the complex PTUCo at range of temperatures (25-700 °C) with a heating rate of 50 °C/min and the presence of an inert atmosphere of N<sub>2</sub> gas and a flow rate of 30 mL/min. Figure 5 showed TGA-DTG thermogram for PTUCo complex. Through this technique, some thermal functions were calculated, such as the stages of dissociation of the material, the temperature at which the material disintegrates, the rate of dissociation rate, in addition to the remainder after the dissolution process, In Figure (5) the TGA and DTG pyrolysis curve shows the PTUCo complex, it has five phases of dissociation at a temperature of 234.69 °C, the second at 403.81 °C and the third at a temperature of 455.70 °C, while the fourth at a temperature of 553.71 °C .



**Figure 5:** TGA-DTG thermogram for PTUCo complex.

The last one was at a temperature of 632.50 °C and found that the value of  $T_s^*$  is at a temperature of 440 °C and has a char content through the TGA curve or the residue at a temperature of 600 °C estimated at 75% and the rate of dissociation rate of 1.961%/min, as it is through a curve follow-up TGA at a dissociation rate of approximately 11.78%. The loss of  $N_2$  and  $H_2$  gases from the two ligand thiourea, and at approximately 25% of the loss, there is a loss of carbon monoxide, hydrogen gas and carbon sulfide CS [43, 44].

#### 4. Corrosion study:

The carbon steel alloy employed in this study was C1010 type. The alloy composition is shown in Table 3 below. The composition is obtained by analysis of alloy from university of Basrah, college of engineering.

**Table 3. Carbon steel composition (C1010).**

Element	C	Mn	Cr	P	S	Cu	Si	As	Ni	Fe
w/w%	0.13	0.30	0.10	0.05	0.04	0.30	0.37	0.08	0.30	Balance

##### 4.1. Preparation of working electrode

Table 3 represent the composition of the specimens that used to evaluate (PTUCo) as corrosion inhibitor for carbon steel C1010. the specimens of carbon steel (C1010) was studied as strips with dimensions of (3.1) Cm × (1.15) Cm × (0.15) Cm as length, width and thickness respectively. The dimensions are measured by Vernier with sensitivity of (1) mm. the strips were grinded by silicon carbide with grades 120, 180, 320, 400 and 600 respectively. At each step of grinding the specimen washed by cooling water to reduce the raising in temperature and to prevent the adhesion of the particles of grinding papers taking into account each grinding process is perpendicular on the other to remove any impurities on the alloy surface. Then specimens were washed by water and soap to remove the impurities, and after that the residue of soap was removed by washing with distilled water and ethanol, finally washed by acetone and dried by air to polish by polishing device. The specimen was polished through disc rotator covered by shamwa, alumina  $Al_2O_3$  was added on the polishing disc to polish the sample very well to be smooth as mirror. Then the samples were washed again by distilled water, ethanol and acetone then dried by air. finally, the strips kept in desiccator to prevent them against the moisture.

##### 4.2. Electrochemical cells, potentiodynamic method (Tafel plot), and solution preparation.

In this study, the electrochemical cell in the corrosion test consisted of a 75 mL vessel connected to three electrodes: platinum electrode, carbon steel specimen, and saturated calomel electrode as counter, working, and reference electrodes, respectively. used Five concentrations for PTUCo complex were prepared include (1,2,3,4 and 5) ppm to study the effect of concentration of the complex on the corrosion of surface of C1010 alloy at 25 °C by using the electrochemical method (Tafel plot method) separately to prepare. The effect of temperature on the corrosion reaction in the presence and absence of optimal and minimal PTUCo concentrations was studied at 25, 35, 45, and 55°C in 0.1 M HCl as a corrosive agent. Potentiodynamic and polarization measurement is a commonly used technique to measure corrosion resistance and various functions and determine the current density versus the electric potential through a setup of open circuit potential (OCP) for 25 min. The polarization curve can then be acquired by scanning the potential range between -250 mV and +250 mV (vs. OCP) by using a computer for potentiostat/galvanostat at a scanning rate of 10 mV  $S^{-1}$ . Various parameters such as corrosion current density ( $I_{corr}$ ), corrosion potential ( $E_{corr}$ ), cathodic ( $\beta_c$ ) and anodic ( $\beta_a$ ). shows a slight drift in the OCP values towards the negative showing the presence of CoPTU inhibitor, this behavior is attributed to adsorption of the inhibitor or/and deposition of the products of the corrosion reaction on the C1010 alloy.

## 5. Results and discussion

Figure 6 shows Tafel plots for Five concentrations of PTUCo complex relative to blank (corrosive environment of 0.10M of (HCl).

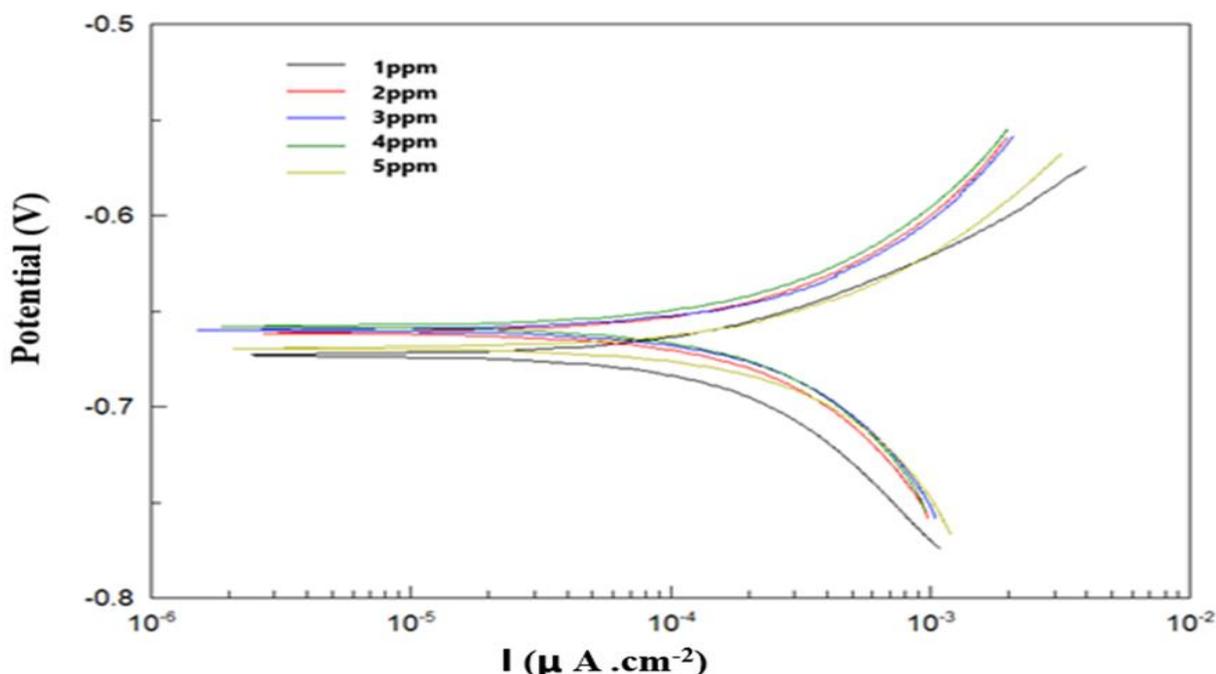


Figure 6: Tafel plots for carbon steel alloy C1010 in presence of different concentration of PTUCo complex at 25 °C.

The electrochemical data were summarized in Table 4 below.

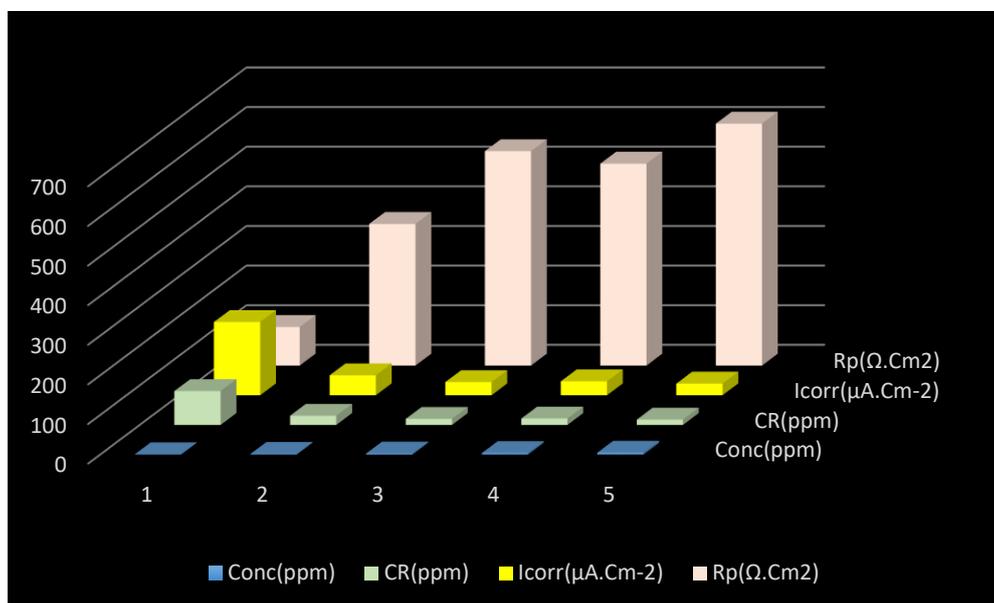
Table 4: The electrochemical data for the corrosion of C1010 alloy surface in presence of different concentrations of PTUCo relative to blank at 25 °C.

Comp.	Conc. ppm	$E_{\text{corr}}$ mV	$\beta_a$ mV.decade <sup>-1</sup>	$\beta_c$ mV. decade <sup>-1</sup>	$R_{\text{ct}}$ $\Omega$ .Cm <sup>2</sup>	$I_{\text{corr}}$ $\mu$ A.Cm <sup>-2</sup>	CR mpy	Effe. %
HCl	3650	- 659	171.27	-333.06	26.28	685.06	317.23	-
PTUCo	1	- 674	76.61	-147.37	97.37	184.87	85.61	72.96
	2	- 675	474.03	-440.48	357.45	50.36	23.58	92.58
	3	- 677	334.64	-274.71	541.13	33.26	15.40	95.08
	4	- 680	434.49	-366.58	509.66	35.32	16.36	94.77
	5	- 681	424.04	-356.89	610.64	29.48	13.65	95.63

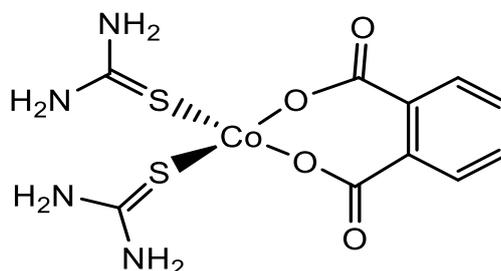
It was depicted from Figure 6 and Table 4, the presence of the complex PTUCo was reduced the corrosion rate for the surface of C1010 alloy at all its concentrations compared with case in presence of blank because the corrosion current density was reduced, the resistance polarization of the alloy was increased as shown in Figure 7, the inhibition efficiency was raised as the concentration of the inhibitor increased to (5) ppm where the damping efficiency is 95.63% [45, 46], the irregular efficiency values between 3ppm to 5ppm concentration can be assigned to is due to the solubility of the inhibitor studied in the acid medium.

Furthermore, the corrosion potential of the alloy in the presence of the corrosive environment  $E_{\text{corr}}$  is (- 659) mV compared with the presence of studied concentrations  $E_{\text{corr}}$  of the inhibitor values were shifted compared with blank by less than 89mV that indicate the inhibitor behave as mixed inhibitor [47, 48] and both  $\beta_a$  and  $\beta_c$  values were shifted compared with these in blank insisted that the anodic dissolution in anode and hydrogen evolution in cathode were be controlled [49]. It is also possible to suggest that

the high efficiency of inhibition and its convergence within the higher concentrations is due to the complex shape of the complex (PTUCo) which was deduced from magnetic sensitivity calculations as a tetrahedral magnetic bar providing four amine groups (NH<sub>2</sub>) and two groups of the thiourea for each complex molecule in addition to the phthalate ion in which Adsorption sites such as benzene ring and the two groups of carbonyl (C = O) as shown in [Figure 8](#) below.



**Figure 7:** The relation between the concentration of the inhibitors and the electrochemical data for the alloy’s surface (C1010).



**Figure 8:** explained the relation between these data and the concentration of the inhibitor.

The efficiency is calculated as in the following equation [50]:

$$efficiency\% = \frac{CR_{uninhib} - CR_{inhib}}{CR_{uninhib}} \times 100 \dots\dots\dots 2$$

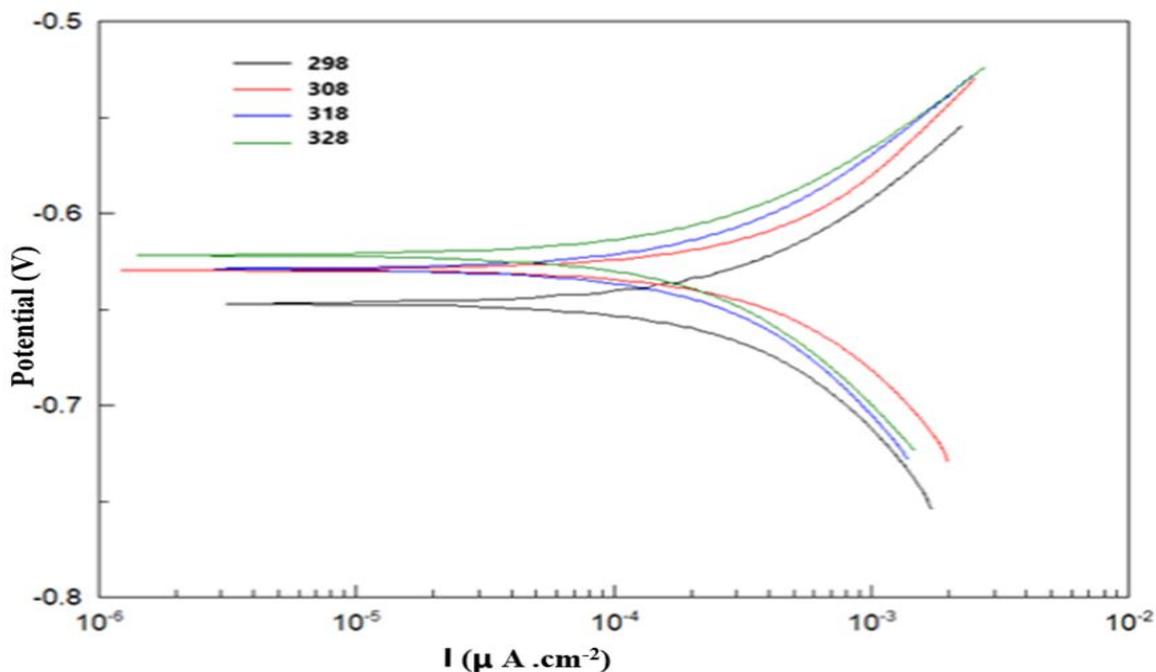
Where,  $CR_{uninhib}$  and  $CR_{inhib}$  are the corrosion rate of the C1010 alloy in the absence and presence of the inhibitors respectively.

**5.2. Study the effect of temperature on the corrosion rate of the C1010 alloy:**

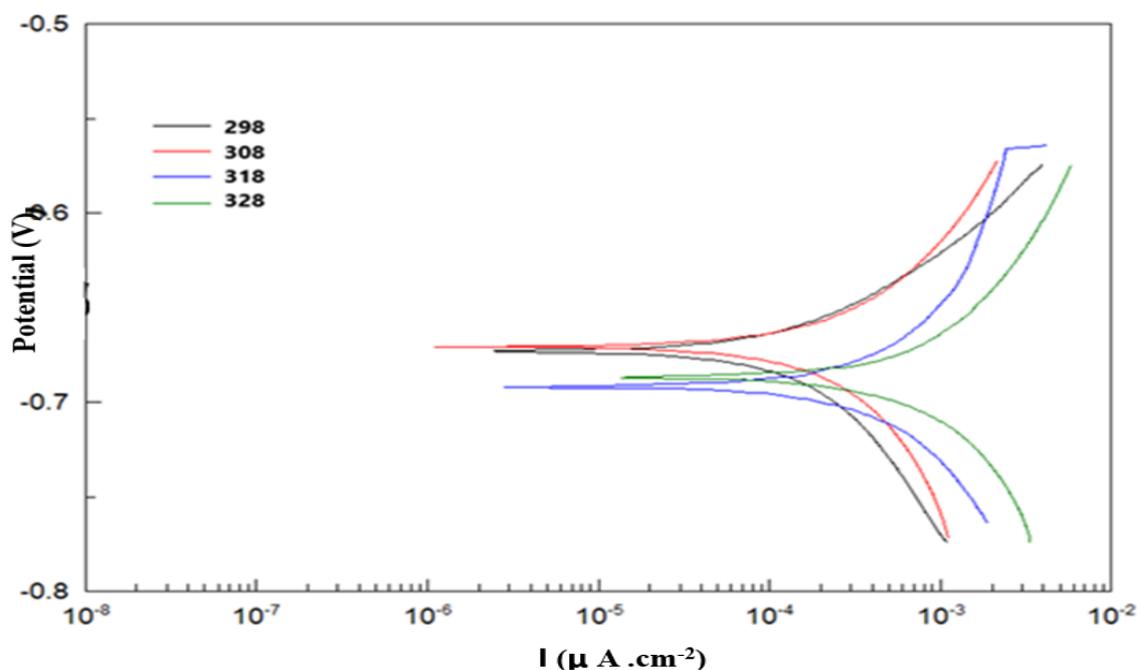
The effect of temperature on the corrosion reaction on the surface of the mentioned alloy was studied at 298, 308, 318 and 328 K by using Tafel plot methodes at an minimal concentration (1ppm) and at optimal concentration (5ppm). [Figures 9, 10 and 11](#) below depicted Tafel plots for C1010 in absence and presence of a minimal and an optimal concentration of PTUCo as inhibitor. The electrochemical data for these cases were obtained and summerized in [Tabel 5](#) as shown below.

Where, Blank is corrosive environment (0.1M HCl), its concentration in ppm is equal to 3650 ppm. As shown from [Table 6](#), the raising of temperature from 298K (25 °C) to 328K(55 °C) the corrosion rate is increased, because the corrosion current increased then, the resistance polarization and inhibition

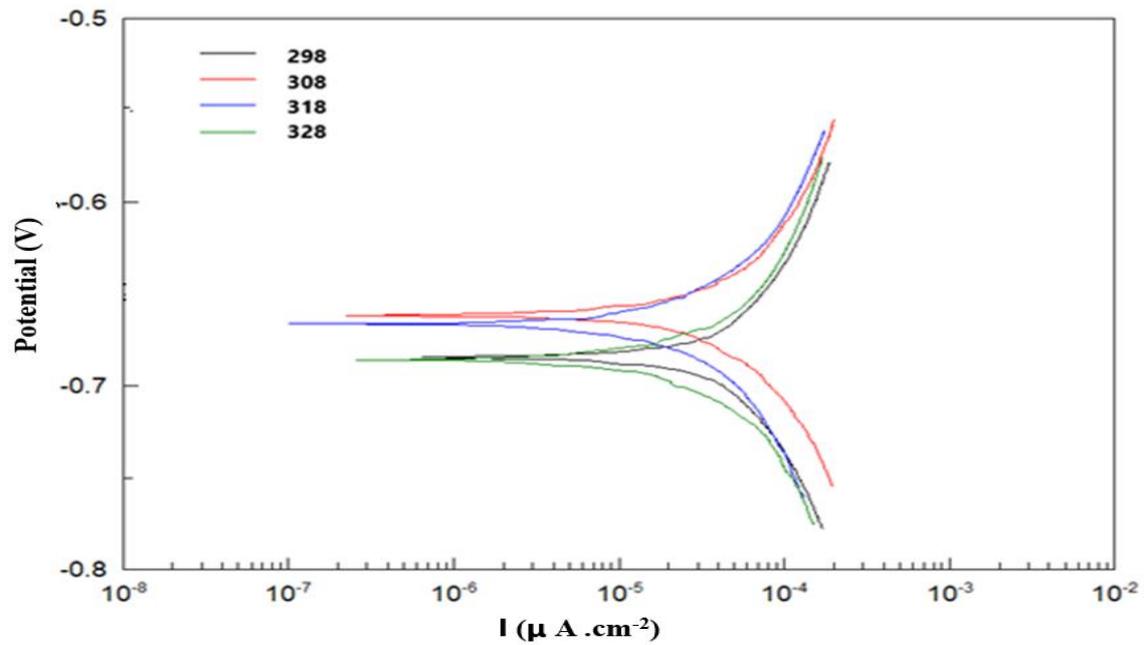
efficiency of the inhibitor were reduced in both cases (minimal and optimal concentrations) because the protective film of the inhibitor began to dissolved on surface of the alloy where, the corrosive species were attack the surface of. The disparity in efficiencies' values due to the variation of desorption phase relative to the temperature ; a decrease in inhibition efficiencies with the increase in temperature might be due to weakening of physical adsorption sites while retarding the chemisorption sites [51] and a significant decrease is also observed compared to the decrease in efficiency of inhibition using the optimum concentration with increasing temperature within the aforementioned thermal range.



**Figure 9:** Tafel plots for carbon steel alloy C1010 in presence of corrosive environment of 0.10M HCl at different temperature.



**Figure 10:** Tafel plots for carbon steel alloy C1010 in presence of the minimal concentration (1ppm) of PTUCo complex at different temperature.

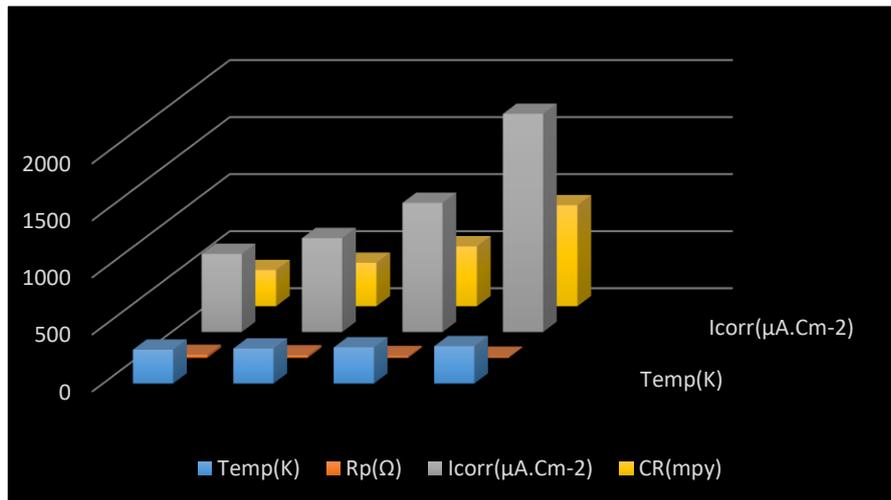


**Figure 11:** Tafel plots for carbon steel alloy C1010 in presence of the optimal minimal concentration (5ppm) of PTUCo complex at different temperature.

**Table 5:** The electrochemical data for the corrosion of C1010 alloy surface in presence of minimal concentration (1ppm) and optimal concentration (5ppm) for PTUCo at different temperatures relative to blank.

Comp.	Conc. ppm	Temp. K	$E_{corr}$ mV	$\beta_a$ mV.decade	$\beta_c$ mV.decade	$R_{ct}$ $\Omega.Cm^2$	$I_{corr}$ $\mu A.Cm^{-2}$	CR mpy	Effe.%	$\theta$
HCl	3650	298	- 659	171.27	-333.06	26.28	685.06	317.23	-	
HCl		308	- 670	370.54	-825.15	21.86	823.32	381.26	-	
HCl		318	- 674	56.45	-186.37	15.87	1132.1	525.16	-	
HCl		328	- 678	193.53	-1165.40	9.41	1912.3	885.45	-	
PTUCo	1	298	- 674	76.61	-147.37	97.37	184.87	85.61	72.96	0.7296
PTUCo	1	308	- 671	161.31	-329.92	73.371	245.33	113.61	70.12	0.7012
PTUCo	1	318	- 691	473.69	-271.22	40.978	439.26	203.41	61.13	0.6113
PTUCo	1	328	- 687	130.81	-133.44	22.49	800.34	370.62	58.18	0.5818
PTUCo	5	298	- 681	424.04	-356.89	610.64	29.48	13.65	95.63	0.9563
PTUCo	5	308	- 676	187.35	-217.51	86.17	208.88	96.79	74.53	0.7453
PTUCo	5	318	- 681	409.59	-430.11	51.89	346.88	160.63	69.26	0.6926
PTUCo	5	328	- 691	156.92	-785.45	22.04	816.82	378.29	57.31	0.5731

Therefore, it is preferable to use the optimal concentration of inhibitor (PTUCo) with an optimal concentration of (5) ppm and is observed in both the two cases of the values of the Tafel anode and cathode constants are that they are in a change and fall indication of a decrease in the control mechanisms of the anode and cathode reactions [45, 52]. One of the values of corrosion efforts is that the inhibitor is still conducting a double inhibitor even with a high temperature. in Figure 12 the effect of temperature on corrosion rate and other electrochemical parameters can be shown.



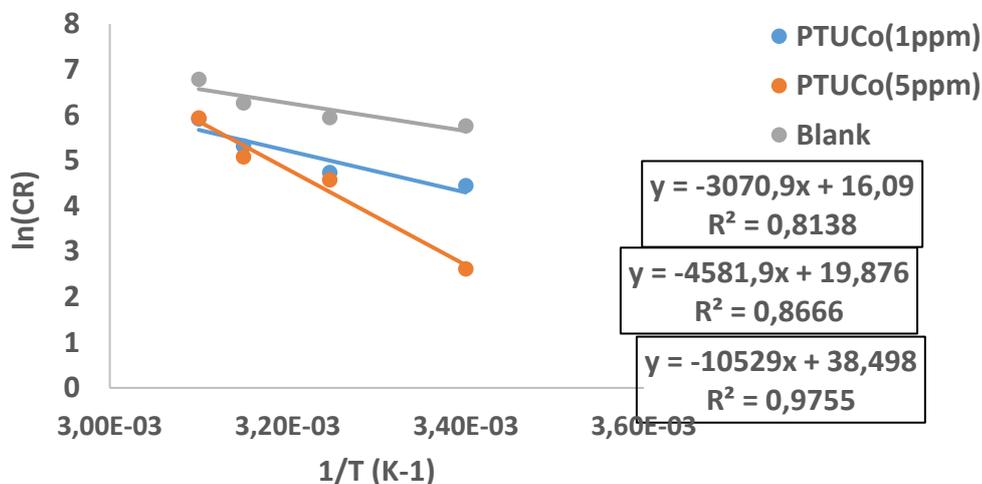
**Figure 12:** The effect of temperature on the electrochemical parameters on the 1010 alloy in absence of the inhibitor.

### 5.6. Calculation of kinetic parameters for corrosion reaction of alloy:

In this study, kinetic parameters like activation of energy  $E_a^*$  in  $\text{kJ.mol}^{-1}$ , enthalpy of activation  $\Delta H^*$  in  $\text{kJ.mol}^{-1}$  and entropy of activation  $\Delta S^*$  in  $\text{J.K}^{-1}.\text{mol}^{-1}$  were calculated for the optimal and minimal concentrations to explain the behavior of corrosion reaction on the alloy in presence and absence of the inhibitor. Firstly, activation energy was calculated according to Arrhenius equation as in equation 8 below [9, 53, 54]:

$$\ln CR = \ln A - \frac{E_a^*}{RT} \dots \dots \dots 3$$

Where, A is Arrhenius Pre-exponential and CR is corrosion rate in pmy. Thus, plotting the relationship between  $\ln CR$  against  $\frac{1}{T}$  to give a straight line with slope equal to  $(-\frac{E_a^*}{R})$  as in Figure 13 below:

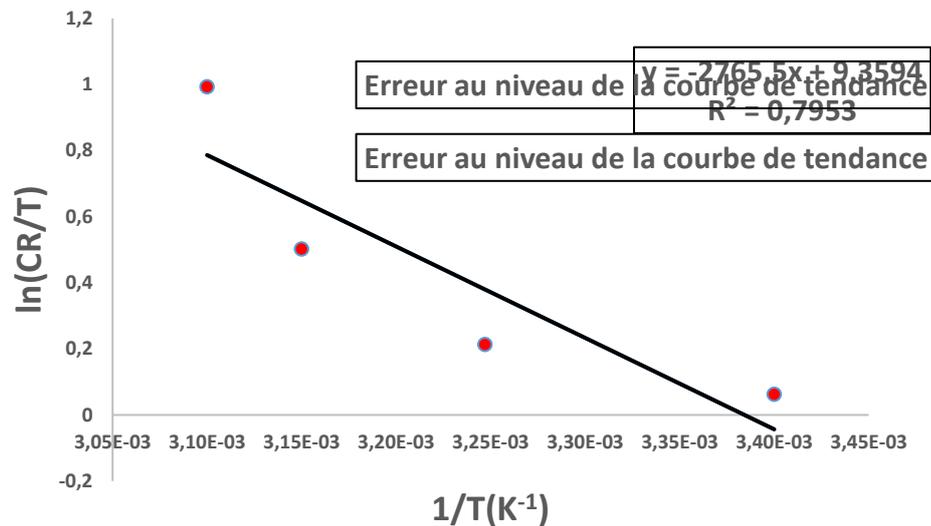


**Figure 13:** Arrhenius relationship for the corrosion reaction on the surface of C1010 alloy in absence and presence of 1 and 5 ppm of PTUCo.

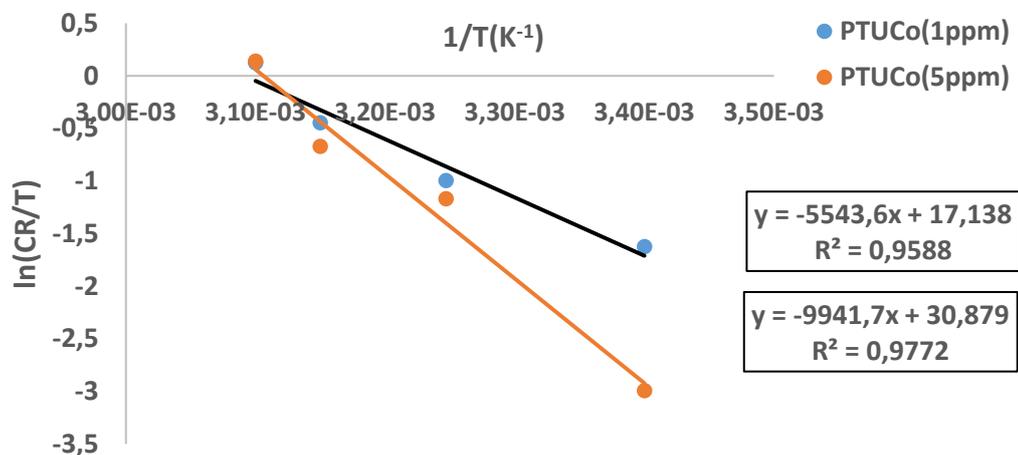
The enthalpy and entropy of activation were calculated as in equation 9 below [52, 54, 55]:

$$\ln\left(\frac{CR}{T}\right) = \ln\frac{R}{Nh} + \frac{\Delta S^*}{R} - \frac{\Delta H^*}{RT} \dots \dots \dots 4$$

Where, N is Avogadro's number is equal to  $6.023 \times 10^{23} \text{mol}^{-1}$  and h is Plank's constant is equal to  $6.625 \times 10^{-34} \text{J.s}$ . thus, plotting of  $\ln\left(\frac{CR}{T}\right)$  against  $\frac{1}{T}$  give a straight line, its slope equal to  $\frac{-\Delta H^*}{R}$  and the intercept equal to  $\left(\ln\frac{R}{Nh} + \frac{\Delta S^*}{R}\right)$  as in Figures 14 and 15 below :



**Figure 14:** calculation of enthalpy and entropy of activation for the corrosion reaction on the surface of C1010 alloy in presence of corrosive environment only.



**Figure 15:** calculation of enthalpy and entropy of activation for the corrosion reaction on the surface of C1010 alloy in absence and presence of 1 and 5 ppm of PTUCo.

The kinetic parameters were summarized in [Table 7](#) below:

**Table 7:** Kinetic parameters for the corrosion reaction on the surface of C1010 alloy in absence and presence of PTUCo inhibitor.

Comp.	Conc. ppm	$E_a$ $\text{kJ.mol}^{-1}$	$A$ $\text{s}^{-1}$	$\Delta H^*$ $\text{kJ.mol}^{-1}$	$\Delta S^*$ $\text{J.mol}^{-1}.\text{K}^{-1}$	$\Delta G^*$ $\text{kJ.mol}^{-1}$
HCl	3650	25.53	$9.72 \times 10^6$	22.99	-119.73	58.67
PTUCo	1	38.09	$4.29 \times 10^8$	46.09	-55.06	62.50
	5	87.54	$5.24 \times 10^{16}$	82.66	59.19	65.02

[Table 7](#) depicted that the energy of activation in presence of PTUCo inhibitor is greater than in absence of inhibitor especially in presence of optimal concentration (5ppm), which means that the corrosion reaction of the carbon steel iron alloy in the absence of the inhibitor is fast compared with the presence of the inhibitor. Furthermore, in case of presence the optimal concentration, the corrosion reaction became very slow that corresponding with the higher damping efficiency than in case of a minimal

concentration i.e., the inhibition of the optimal inhibitor on the alloy surface was forming a higher protective layer on the surface of the alloy [56, 57]. On the other hand, the enthalpy of activation corrosion reaction  $\Delta H^*$  values were positive and increased in presence of the inhibitor especially in case of the optimal concentration that confirm the dropping of the inhibition efficiencies as the temperature was raised. This confirms that the process of adsorption of inhibitor is more chemical than physical, in other words that the chemical desorption separation needs to heat to get faster [50, 58]. It is also noticed through Table 7 that the values of the Arrhenius coefficient (A) increase with the presence of the inhibitor, especially at the optimal concentration, it is worth noting that the Arrhenius coefficient indicates the coefficient of vibration of the interacting particles i.e., the corrosive species and the surface of alloy in absence of the inhibitor, this coefficient was raised in the presence of the inhibitor that can be attributed to the increasing the vibration of the reaction system i.e., (corrosion product (none porous hydrated iron oxide), inhibitor molecules and the surface of alloy) to form the activated complex which tends to form a protective layer [53,54]. On the other hand, the values of the activation entropy is negative in case of absence the inhibitor (-119.73) J.mol<sup>-1</sup>.K<sup>-1</sup> means that the corrosion products tends to be stable and regular on the surface of alloy. The negative value then tends to be reduced in case of the presence of a minimal concentration (-55.06) J.mol<sup>-1</sup>.K<sup>-1</sup> reached to be positive value (59.19) J.mol<sup>-1</sup>.K<sup>-1</sup> when the optimal concentration of the inhibitor is present on the surface of alloy, this can be attributed to increase the instability of corrosion products when the certain inhibitor was adsorbed on the surface of alloy causing the increasing the entropy to combine between each other i.e., the process of adsorption of the inhibitor affects the corrosion reaction by expelling the larger number of corrosive molecules with water molecules, which increases the randomness of the reaction, leading to the formation of an adsorbent layer that reduces the corrosion process [58-60].

## Conclusions

The cobalt complex (PTUCo) has a tetrahedral geometrical shape paramagnetic, which confirms the replacement of two ligands from thiourea versus the one ligand of the phthalate ion. The synthesized complex PTUCo can be used as corrosion inhibitor for corrosive environment of 0.10M of HCl at very little concentration i.e., 5 ppm with efficiency 95.63%. Its behavior is mixed inhibitor. Where, the inhibitor PTUCo raised the activation energy for the corrosion reaction on the surface of C1010 alloy. The mechanism of hydrogen evolution in the cathode and anodic dissolution in the anode were controlled in presence of this inhibitor.

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